

WHAT IS CLAIMED IS:

1. A method of determining at least one characteristic of a tire selected from: the x component, y component, and z component of a resultant of forces which are exerted by the road on the contact area of a tire, the self-alignment torque generated by the tire, the camber and the pressure, the method comprising the steps of measuring stresses in at least one bead of the tire at at least three fixed points in space, and deriving the characteristic from said at least one measurement.
2. The method according to Claim 1, wherein the measurement of the stresses is performed in a rubber component whose Young's modulus is more than 5 MPa at 10% strain.
3. The method according to Claim 1, the said three fixed points being selected such that:
  - one of the points corresponds to the azimuth of the center of the contact area or the azimuth of the point opposite to the contact area; and,
  - two other points are symmetrical with respect to a vertical plane passing through the center of the contact area.
4. The method according to Claim 3, in which, the measurement azimuths being selected symmetrically with respect to the azimuth of the center of the contact area ( $180^\circ + \alpha$  and  $180^\circ - \alpha^\circ$ ), with  $\alpha$  not equal to  $0^\circ$  or  $180^\circ$ ,  $V_1^1$  and  $V_2^1$  being values measured at these azimuths on a first bead and  $V_1^2$  and  $V_2^2$  being the values measured at these azimuths on a second bead, an estimate of the component  $F_x$  is provided by  $f_x(a_1 V_1^1 + a_2 V_2^1 + b_1 V_1^2 + b_2 V_2^2)$ , where  $a_1$ ,  $a_2$ ,  $b_1$  and  $b_2$  are positive real coefficients and  $f_x$  is a monotonic continuous function.
5. The method according to Claim 3, in which, the measurement azimuths being selected symmetrically with respect to the azimuth of the center of the contact area ( $180^\circ + \alpha$  and  $180^\circ - \alpha^\circ$ ), with  $\alpha$  not equal to  $0^\circ$  or  $180^\circ$ ,  $V_1^1$  and  $V_2^1$  being values measured at these azimuths on the first bead and  $V_1^2$  and  $V_2^2$  being values measured

at these azimuths on the second bead, an estimate of the component  $F_z$  is provided by  $f_z(c_1 V_1^1 - c_2 V_2^1 + d_1 V_1^2 - d_2 V_2^2)$ , where  $c_1$ ,  $c_2$ ,  $d_1$  and  $d_2$  are positive real coefficients and  $f_z$  is a monotonic continuous function.

6. The method according to Claim 3, in which, the measurement azimuths being selected symmetrically with respect to the azimuth of the center of the contact area ( $180^\circ + \alpha$  and  $180^\circ - \alpha^\circ$ ), with  $\alpha$  not equal to  $0^\circ$  or  $180^\circ$ ,  $V_1^1$  and  $V_2^1$  being values measured at these azimuths on the first bead and  $V_1^2$  and  $V_2^2$  being values measured at these azimuths on the second bead, an estimate of the self-alignment torque  $N$  is provided by  $f_n(e_1 V_1^1 + e_2 V_2^1 - f_1 V_1^2 - f_2 V_2^2)$ , where  $e_1$ ,  $e_2$ ,  $f_1$  and  $f_2$  are positive real coefficients and  $f_n$  is a monotonic continuous function.
7. The method according to Claim 3, in which, the measurement azimuths being selected symmetrically with respect to the azimuth of the center of the contact area ( $180^\circ + \alpha$  and  $180^\circ - \alpha^\circ$ ), with  $\alpha$  not equal to  $0^\circ$  or  $180^\circ$ ,  $V_1^1$  and  $V_2^1$  being values measured at these azimuths on the first bead and  $V_1^2$  and  $V_2^2$  being values measured at these azimuths on the second bead, an estimate of the component  $F_y$  is provided by  $f_y(g_1 V_1^1 - g_2 V_2^1 - h_1 V_1^2 + h_2 V_2^2)$ , where  $g_1$ ,  $g_2$ ,  $h_1$  and  $h_2$  are positive real coefficients and  $f_y$  is a monotonic continuous function.
8. The method according to Claim 3, in which, the measurement azimuths being selected symmetrically with respect to the azimuth of the center of the contact area ( $180^\circ + \alpha$  and  $180^\circ - \alpha^\circ$ ), with  $\alpha$  not equal to  $0^\circ$  or  $180^\circ$ , and  $V_1$  and  $V_2$  being values measured at these other azimuths, an estimate of  $F_z$  is provided by  $f_z(r_2 V_2 - r_1 V_1)$ , where  $r_1$  and  $r_2$  are positive real coefficients and  $f_z$  is a monotonic continuous function.
9. The method according to Claim 3, in which, one of the azimuths corresponding to the middle of the contact area (azimuth  $180^\circ$ ) and  $V_c$  being a value measured at this azimuth, the other measurement azimuths being selected symmetrically with respect to the azimuth of the center of the contact area ( $180^\circ + \alpha$  and  $180^\circ - \alpha^\circ$ ), with  $\alpha$  not equal to  $0^\circ$  or  $180^\circ$ , and  $V_1$  and  $V_2$  being values measured at these other azimuths,

an estimate of  $F_y$  is provided by  $f_y(s_c V_c - (s_1 V_1 + s_2 V_2))$ , where  $s_1$ ,  $s_2$  and  $s_c$  are positive real coefficients and  $f_y$  is a monotonic continuous function.

10. The method according to Claim 3, in which, one of the azimuths corresponding to the middle of the contact area (azimuth  $180^\circ$ ) and  $V_c$  being a value measured at this azimuth, the other measurement azimuths being selected symmetrically with respect to the azimuth of the center of the contact area ( $180^\circ + \alpha$  and  $180^\circ - \alpha$ ), with  $\alpha$  not equal to  $0^\circ$  or  $180^\circ$ , and  $V_1$  and  $V_2$  being values measured at these other azimuths, an estimate of  $F_x$  is provided by  $f_x(u_c V_c + u_1 V_1 + u_2 V_2)$ , where  $u_1$ ,  $u_2$  and  $u_c$  are positive real coefficients and  $f_x$  is a monotonic continuous function.
11. The method according to Claim 1, wherein to estimate camber angle, the method comprises determining a difference in stresses being exerted in each of the beads on the basis of the measurements of stresses in the beads.
12. The method according to Claim 1, wherein, to estimate pressure a contribution due to the pneumatic behaviour separate from a contribution due to structural behaviour is determined on the basis of the measurements of stresses in the beads.
13. A method of determining at least one characteristic of a tire selected from: the x component, y component and z component of a resultant of forces which are exerted by the road on the contact area of the tire, the self-alignment torque generated by the tire, the camber, and the pressure, the method comprising the steps of:
  - determining measurement azimuths and collecting values for circumferential shear stress in a bead on at least one side of the tire while soliciting varied stresses on the tire, which stresses are selected to cover the full range in which evaluation of the at least one selected characteristic will be permitted in normal use, the solicited stresses selected to create all the couplings expected during normal use,
  - reading measured values for circumferential shear stress in the bead and
  - reading values of the at least one characteristic associated with the measured values to form a training base, the values of the at least one characteristic being obtained through measurement means different from the means for the measured values,

determining coefficients of a transfer function for establishing a link between the measured values and the values of the at least one selected characteristic on the basis of the training base, and,

testing the transfer functions by making and comparing estimates of the at least one selected characteristic with the values obtained by different measurement means.

14. The method of determination according to Claim 13, in which the transfer function is a network having one layer of hidden neurons and one layer of output neurons.